



# **DPA-2025-OCTOBER-2223**

## **Delivery Point Network Study**

Published on 03/27/2026

By SPP Engineering, Transmission Services

# REVISION HISTORY

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| DATE OR<br>VERSION NUMBER | AUTHOR | CHANGE<br>DESCRIPTION | COMMENTS |
|---------------------------|--------|-----------------------|----------|
| 03/27/2026                | SPP    | Original              |          |
|                           |        |                       |          |
|                           |        |                       |          |

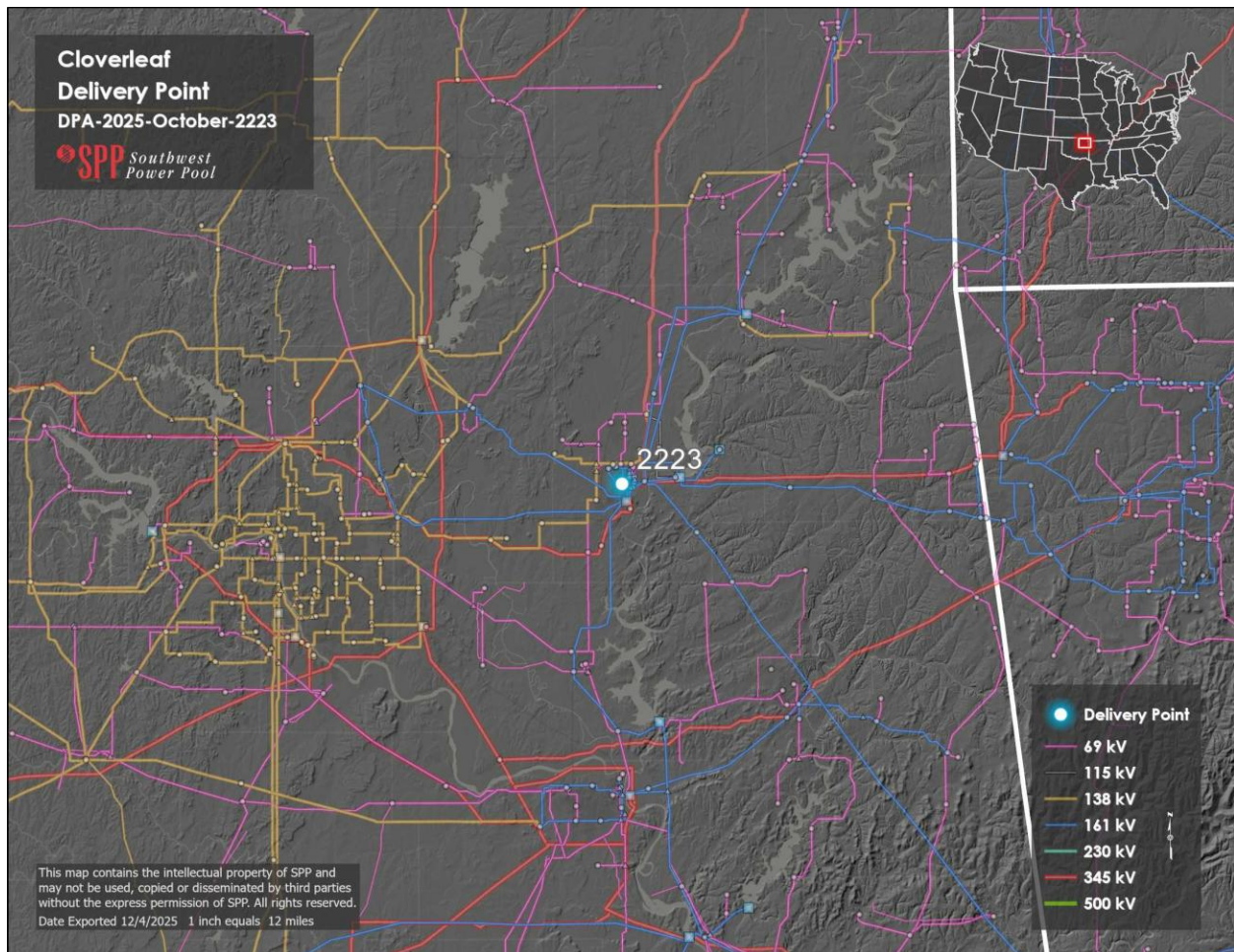
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## SECTION 1: INTRODUCTION

This report outlines the results of an evaluation of regional transmission impacts from delivery point request DPA-2025-October-2223. The requesting entity plans to add a new delivery point called Cloverleaf with an in-service date of 12/01/2026. The Cloverleaf delivery point is in the Grand River Dam Authority (GRDA) Transmission System.



The load flow models used for the evaluation were 2025 Integrated Transmission Planning (ITP) base reliability models. Southwest Power Pool (SPP) performed an Alternating Current (AC) contingency analysis on these models using PSS@E.

## SECTION 2: STUDY METHODOLOGY

### OBJECTIVE

The purpose of this study was to determine the regional Transmission System impacts within the SPP footprint due to the new load served by GRDA. SPP performed a Delivery Point Network Study (DPNS) with the configurations shown in Table 2-1 below.

### STUDY PROCESS

- Model Assumptions
  - 2025 ITP Base Reliability Model Series
    - Model years 2026, 2029, and 2034
    - Summer Peak (2029S and 2034S), Winter Peak (2026W, 2029W, and 2034W), and Light Load (2029L, and 2034L)
  - 2025 ITP Short Circuit Model Series
    - 2029 Summer Max Fault
  - 2025 Transmission System Planning (TSP) Dynamic Model Series
    - 2034 Summer Peak Base and Change Cases

**Table 2-1: Study Cases**

| Case Name                 | Study Year | Season      | Scenario         | Load (MW/MVAR)         |
|---------------------------|------------|-------------|------------------|------------------------|
| 2025ITPFinal-26W.sav      | 2026       | Winter Peak | Base Reliability | Base Case              |
| 2025ITPFinal-29L.sav      | 2029       | Light Load  | Base Reliability | Base Case              |
| 2025ITPFinal-29S.sav      | 2029       | Summer Peak | Base Reliability | Base Case              |
| 2025ITPFinal-29W.sav      | 2029       | Winter Peak | Base Reliability | Base Case              |
| 2025ITPFinal-34L.sav      | 2034       | Light Load  | Base Reliability | Base Case              |
| 2025ITPFinal-34S.sav      | 2034       | Summer Peak | Base Reliability | Base Case              |
| 2025ITPFinal-34W.sav      | 2034       | Winter Peak | Base Reliability | Base Case              |
| 2025ITPFinal-26W_2223.sav | 2026       | Winter Peak | Base Reliability | Cloverleaf = 20/2.85   |
| 2025ITPFinal-29L_2223.sav | 2029       | Light Load  | Base Reliability | Cloverleaf = 375/53.43 |
| 2025ITPFinal-29S_2223.sav | 2029       | Summer Peak | Base Reliability | Cloverleaf = 375/53.43 |
| 2025ITPFinal-29W_2223.sav | 2029       | Winter Peak | Base Reliability | Cloverleaf = 375/53.43 |
| 2025ITPFinal-34L_2223.sav | 2034       | Light Load  | Base Reliability | Cloverleaf = 375/53.43 |
| 2025ITPFinal-34S_2223.sav | 2034       | Summer Peak | Base Reliability | Cloverleaf = 375/53.43 |
| 2025ITPFinal-34W_2223.sav | 2034       | Winter Peak | Base Reliability | Cloverleaf = 375/53.43 |

- Steady State Analysis
  - Assumptions (consistent with the ITP analysis)
    - AC contingency analysis on all load flow models using PSS®E
    - Monitored Elements
      - SPP facilities 69 kV and above
      - First-tier companies 100 kV and above
    - Contingencies (consistent with the ITP analysis)
      - Provided for the ITP by SPP members and first-tier companies
    - Apply SPP Criteria and National American Electric Reliability Corporation (NERC) reliability standards
  - Compare thermal and voltage violations that occur with and without the Cloverleaf delivery point change to determine thermal and voltage violations resulting from the load addition to the Transmission System.
- Dynamics Analysis
  - Assumptions
    - 2025 TPL Dynamics Model Series
      - 2034 Summer Peak Base and Change Cases
  - Analyses
    - Fast Fault Screening using Physical and Operational Margins Studio
- Short Circuit Analysis
  - Assumptions
    - Used 2024 Final ITP Short Circuit models (2029 Summer Max Fault)
      - Placed all available facilities in service
        - Generation
        - Transmission lines
        - Transformers
        - Buses
      - Short Circuit Output
        - Physical
      - Short Circuit Coordinates
        - Polar
      - Short Circuit Parameters
        - 3 Phase
      - FLAT – classical fault analysis conditions
  - Analyses
    - Three-phase fault

## SECTION 3: RESULTS OF ANALYSIS

### POTENTIAL THERMAL AND VOLTAGE VIOLATIONS

The analysis identified potential thermal and voltage violations resulting from the new load at the Cloverleaf delivery point. Table 3-1 details the potential thermal violations and Table 3-2 details the potential voltage violations resulting from the load addition.

**Table 3-1: Potential Thermal Violations**

| Year | Voltage Level (kV) | Facility Name           | Contingency Name        | Rate A, Rate B (MVA) | Max Flow (MVA) | Change Case Max Loading (%) |
|------|--------------------|-------------------------|-------------------------|----------------------|----------------|-----------------------------|
| 29S  | 161                | GRDA1 5 - WMAIN ST5 - 1 | MAID 5 - PATROLRD 5 - 1 | 713/837              | 847.881        | 101.3                       |
| 34S  | 161                | GRDA1 5 - WMAIN ST5 - 1 | MAID 5 - PATROLRD 5 - 1 | 713/837              | 1005.2369      | 120.1                       |
| 34W  | 161                | GRDA1 5 - WMAIN ST5 - 1 | MAID 5 - PATROLRD 5 - 1 | 713/837              | 1004.4         | 120                         |

### SHORT CIRCUIT

SPP performed short circuit analysis for the 2029 Summer Peak with the new load addition. The analysis identified the currents as listed in Table 3-3.

**Table 3-3: Short Circuit Results**

| Season | Model     | Fault       | Bus                | Current (Amps) |
|--------|-----------|-------------|--------------------|----------------|
| 29S    | Max Fault | Three Phase | 1CHOTCT4 16.000    | 13,008         |
| 29S    | Max Fault | Three Phase | 1CHOTCT5 16.000    | 12,392         |
| 29S    | Max Fault | Three Phase | 1CHOTST6 16.000    | 11,082         |
| 29S    | Max Fault | Three Phase | 1CHOTST3 16.000    | 9,766          |
| 29S    | Max Fault | Three Phase | 1CHOTCT1 16.000    | 9,604          |
| 29S    | Max Fault | Three Phase | 1CHOTCT2 16.000    | 9,331          |
| 29S    | Max Fault | Three Phase | 5CHOTEAU1 161.00   | 42,532         |
| 29S    | Max Fault | Three Phase | 7BLACKBERRY 345.00 | 15,476         |
| 29S    | Max Fault | Three Phase | 7SPORTSMAN 345.00  | 24,298         |
| 29S    | Max Fault | Three Phase | 5SPORTSMAN 161.00  | 40,482         |
| 29S    | Max Fault | Three Phase | 2LOWERY 69.000     | 4,677          |
| 29S    | Max Fault | Three Phase | 2PEGGS 69.000      | 6,081          |
| 29S    | Max Fault | Three Phase | 2WAGNERW 69.000    | 4,542          |
| 29S    | Max Fault | Three Phase | 5ELMCRK 161.00     | 13,692         |
| 29S    | Max Fault | Three Phase | 5KETONVL 161.00    | 11,618         |
| 29S    | Max Fault | Three Phase | 5PARK 161.00       | 7,901          |
| 29S    | Max Fault | Three Phase | 1SPORTT1 13.200    | 30,543         |

| Season | Model     | Fault       | Bus                | Current (Amps) |
|--------|-----------|-------------|--------------------|----------------|
| 29S    | Max Fault | Three Phase | 1SPORTT2 13.200    | 30,650         |
| 29S    | Max Fault | Three Phase | 5CDRCRST 161.00    | 10,193         |
| 29S    | Max Fault | Three Phase | 2CDRCRST 69.000    | 7,954          |
| 29S    | Max Fault | Three Phase | 5CHOTEAU2 161.00   | 42,532         |
| 29S    | Max Fault | Three Phase | 1CDRCRSTTR 13.200  | 8,782          |
| 29S    | Max Fault | Three Phase | 2GRAY TP 69.000    | 7,495          |
| 29S    | Max Fault | Three Phase | 5BRIGGSTAP 161.00  | 7,352          |
| 29S    | Max Fault | Three Phase | FT GIB 5 161.00    | 10,490         |
| 29S    | Max Fault | Three Phase | FLINTCR7 345.00    | 16,024         |
| 29S    | Max Fault | Three Phase | SPNKY CK4 138.00   | 28,292         |
| 29S    | Max Fault | Three Phase | INOLATP4 138.00    | 9,439          |
| 29S    | Max Fault | Three Phase | LLAN ET4 138.00    | 24,706         |
| 29S    | Max Fault | Three Phase | CATOOSA4 138.00    | 37,257         |
| 29S    | Max Fault | Three Phase | CATOOSA2 69.000    | 10,848         |
| 29S    | Max Fault | Three Phase | E 11TH ST 4 138.00 | 29,577         |
| 29S    | Max Fault | Three Phase | TERNITP4 138.00    | 20,337         |
| 29S    | Max Fault | Three Phase | PCATSAT4 138.00    | 21,356         |
| 29S    | Max Fault | Three Phase | CAT001-1 13.800    | 17,801         |
| 29S    | Max Fault | Three Phase | OWAS88_4 138.00    | 17,718         |
| 29S    | Max Fault | Three Phase | L GROVE3 115.00    | 17,553         |
| 29S    | Max Fault | Three Phase | KERR_U2 1 13.200   | 17,013         |
| 29S    | Max Fault | Three Phase | KERR_U3 1 13.200   | 16,859         |
| 29S    | Max Fault | Three Phase | PENSA_U1 1 13.200  | 14,253         |
| 29S    | Max Fault | Three Phase | PENSA_U2 1 13.200  | 14,253         |
| 29S    | Max Fault | Three Phase | PENSA_U3 1 13.200  | 14,253         |
| 29S    | Max Fault | Three Phase | PENSA_U4 1 13.200  | 12,041         |
| 29S    | Max Fault | Three Phase | PENSA_U6 1 13.200  | 12,041         |
| 29S    | Max Fault | Three Phase | PENSA_U5 1 13.200  | 12,041         |
| 29S    | Max Fault | Three Phase | SALINA_U1 1 13.400 | 20,786         |
| 29S    | Max Fault | Three Phase | SALINA_U2 1 13.400 | 20,437         |
| 29S    | Max Fault | Three Phase | SALINA_U3 1 13.400 | 20,609         |
| 29S    | Max Fault | Three Phase | SALINA_U4 1 13.400 | 20,269         |
| 29S    | Max Fault | Three Phase | SALINA_U5 1 13.400 | 20,352         |
| 29S    | Max Fault | Three Phase | SALINA_U6 1 13.400 | 20,395         |
| 29S    | Max Fault | Three Phase | GRECCTG_1 20.000   | 19,704         |
| 29S    | Max Fault | Three Phase | GRECSTG_1 21.000   | 83,022         |
| 29S    | Max Fault | Three Phase | CATSAGD4 138.00    | 37,257         |
| 29S    | Max Fault | Three Phase | MAIDTP2 69.000     | 11,995         |
| 29S    | Max Fault | Three Phase | MAID 2 69.000      | 14,806         |
| 29S    | Max Fault | Three Phase | COLINS 5 161.00    | 12,582         |
| 29S    | Max Fault | Three Phase | PENSA 2 69.000     | 13,229         |



| Season | Model     | Fault       | Bus                 | Current (Amps) |
|--------|-----------|-------------|---------------------|----------------|
| 29S    | Max Fault | Three Phase | DRYGULCH5 161.00    | 15,708         |
| 29S    | Max Fault | Three Phase | AFTON 5 161.00      | 8,408          |
| 29S    | Max Fault | Three Phase | KERR GR3 115.00     | 18,674         |
| 29S    | Max Fault | Three Phase | KERR GR5 161.00     | 29,943         |
| 29S    | Max Fault | Three Phase | CATSAGR4 138.00     | 37,257         |
| 29S    | Max Fault | Three Phase | 412SUB 5 161.00     | 11,772         |
| 29S    | Max Fault | Three Phase | CATSAGR5 161.00     | 26,299         |
| 29S    | Max Fault | Three Phase | OKAYGR 5 161.00     | 9,832          |
| 29S    | Max Fault | Three Phase | SILSPWW5 161.00     | 14,872         |
| 29S    | Max Fault | Three Phase | OKAYGR 2 69.000     | 11,944         |
| 29S    | Max Fault | Three Phase | TAHLQH 2 69.000     | 11,167         |
| 29S    | Max Fault | Three Phase | MAID 5 161.00       | 47,640         |
| 29S    | Max Fault | Three Phase | GRDA1 7 345.00      | 26,815         |
| 29S    | Max Fault | Three Phase | CLARMR 5 161.00     | 13,248         |
| 29S    | Max Fault | Three Phase | PENSA 5 161.00      | 13,060         |
| 29S    | Max Fault | Three Phase | TAHLQH 5 161.00     | 8,754          |
| 29S    | Max Fault | Three Phase | GRDA1 5 161.00      | 47,022         |
| 29S    | Max Fault | Three Phase | CPPTAP 2 69.000     | 13,925         |
| 29S    | Max Fault | Three Phase | KETCHUM5 161.00     | 10,553         |
| 29S    | Max Fault | Three Phase | HUNT 2 69.000       | 13,908         |
| 29S    | Max Fault | Three Phase | CLARMR 2 69.000     | 12,626         |
| 29S    | Max Fault | Three Phase | AMERCAST S2 69.000  | 13,647         |
| 29S    | Max Fault | Three Phase | AMERCAST N2 69.000  | 13,602         |
| 29S    | Max Fault | Three Phase | CASTING TAP2 69.000 | 13,909         |
| 29S    | Max Fault | Three Phase | SALINA 5 161.00     | 18,112         |
| 29S    | Max Fault | Three Phase | GRDA17-1 22.800     | 61,433         |
| 29S    | Max Fault | Three Phase | GRDA15-1 22.800     | 21,055         |
| 29S    | Max Fault | Three Phase | WAGNRTP2 69.000     | 7,183          |
| 29S    | Max Fault | Three Phase | CLEORTP2 69.000     | 7,386          |
| 29S    | Max Fault | Three Phase | ADARNE02 69.000     | 4,688          |
| 29S    | Max Fault | Three Phase | WAGNOR 2 69.000     | 7,092          |
| 29S    | Max Fault | Three Phase | REDDEN 2 69.000     | 13,210         |
| 29S    | Max Fault | Three Phase | PRYORCHEM2 69.000   | 13,614         |
| 29S    | Max Fault | Three Phase | WAGNOR 5 161.00     | 9,575          |
| 29S    | Max Fault | Three Phase | COLLINS4 138.00     | 7,890          |
| 29S    | Max Fault | Three Phase | CLARMR 4 138.00     | 13,506         |
| 29S    | Max Fault | Three Phase | KANSATP5 161.00     | 11,627         |
| 29S    | Max Fault | Three Phase | KANSAS 5 161.00     | 11,008         |
| 29S    | Max Fault | Three Phase | GRDA1 2 69.000      | 12,324         |
| 29S    | Max Fault | Three Phase | WMAIN ST5 161.00    | 35,865         |
| 29S    | Max Fault | Three Phase | TONECE7 345.00      | 15,693         |

| Season | Model     | Fault       | Bus                 | Current (Amps) |
|--------|-----------|-------------|---------------------|----------------|
| 29S    | Max Fault | Three Phase | TONECE5 161.00      | 15,419         |
| 29S    | Max Fault | Three Phase | TONECE1 13.200      | 52,424         |
| 29S    | Max Fault | Three Phase | NWMAID5 161.00      | 33,859         |
| 29S    | Max Fault | Three Phase | WAGCTY22 69.000     | 6,524          |
| 29S    | Max Fault | Three Phase | GERALDGAY5 161.00   | 33,232         |
| 29S    | Max Fault | Three Phase | PATROLRD 5 161.00   | 38,737         |
| 29S    | Max Fault | Three Phase | KERR BRK1 5 161.00  | 29,943         |
| 29S    | Max Fault | Three Phase | KERR BRK4 5 161.00  | 29,943         |
| 29S    | Max Fault | Three Phase | GEN-2017-061161.00  | 20,785         |
| 29S    | Max Fault | Three Phase | G17-061XFMR134.500  | 12,012         |
| 29S    | Max Fault | Three Phase | SALNCRK5 161.00     | 18,782         |
| 29S    | Max Fault | Three Phase | CLARMR4 13.800      | 4,729          |
| 29S    | Max Fault | Three Phase | CLARMR1 13.800      | 17,658         |
| 29S    | Max Fault | Three Phase | CLARMR2 13.800      | 16,943         |
| 29S    | Max Fault | Three Phase | GRDA1 1 13.800      | 14,244         |
| 29S    | Max Fault | Three Phase | WAGNOR1 13.800      | 9,467          |
| 29S    | Max Fault | Three Phase | GRDA1 13.800        | 16,058         |
| 29S    | Max Fault | Three Phase | TAHLQH2 1 13.800    | 15,634         |
| 29S    | Max Fault | Three Phase | GRDA2 1 13.800      | 16,959         |
| 29S    | Max Fault | Three Phase | CATTER1 1 13.800    | 5,988          |
| 29S    | Max Fault | Three Phase | CATTER2 1 13.800    | 6,069          |
| 29S    | Max Fault | Three Phase | CATTER3 1 13.800    | 10,079         |
| 29S    | Max Fault | Three Phase | MAITER1 1 13.200    | 32,453         |
| 29S    | Max Fault | Three Phase | MAITER2 1 13.200    | 11,909         |
| 29S    | Max Fault | Three Phase | COLLIN1 1 13.800    | 990            |
| 29S    | Max Fault | Three Phase | COLLIN2 1 13.800    | 13,909         |
| 29S    | Max Fault | Three Phase | COLLIN3 1 13.800    | 9,573          |
| 29S    | Max Fault | Three Phase | PENSA 1 13.800      | 17,474         |
| 29S    | Max Fault | Three Phase | KERR1 1 13.800      | 19,662         |
| 29S    | Max Fault | Three Phase | KERR2 1 13.800      | 19,592         |
| 29S    | Max Fault | Three Phase | OKAY1 13.800        | 13,608         |
| 29S    | Max Fault | Three Phase | TAHLQH1 13.800      | 11,200         |
| 29S    | Max Fault | Three Phase | GEN-2017-073161.00  | 14,568         |
| 29S    | Max Fault | Three Phase | G17-073XFMR134.500  | 8,402          |
| 29S    | Max Fault | Three Phase | G17-073-GSU134.500  | 8,283          |
| 29S    | Max Fault | Three Phase | GREC TAP7 345.00    | 25,815         |
| 29S    | Max Fault | Three Phase | COLNSGR2 69.000     | 10,213         |
| 29S    | Max Fault | Three Phase | LOCSTGV 5 161.00    | 13,381         |
| 29S    | Max Fault | Three Phase | CHOUTEAUUCRK5161.00 | 20,787         |
| 29S    | Max Fault | Three Phase | CUSTDAY2 5 161.00   | 31,504         |
| 29S    | Max Fault | Three Phase | CUSTDAY1 5 161.00   | 31,509         |

| Season | Model     | Fault       | Bus              | Current (Amps) |
|--------|-----------|-------------|------------------|----------------|
| 29S    | Max Fault | Three Phase | HERRON 5 161.00  | 34,819         |
| 29S    | Max Fault | Three Phase | IGLOOV1 5 161.00 | 29,304         |
| 29S    | Max Fault | Three Phase | IGLOOV2 5 161.00 | 29,304         |
| 29S    | Max Fault | Three Phase | IGLOOV 7 345.00  | 21,681         |
| 29S    | Max Fault | Three Phase | 7CLANS 5 161.00  | 8,598          |

### STABILITY

SPP performed a Fast Fault Screening (FFS) using the 2034 Summer Peak for the base case and change case models. The change case models include the Cloverleaf delivery point changes. SPP determined no significant differences in the critical clearing times between the base and change cases. Therefore, a transient stability analysis is not required.

### TRANSMISSION SOLUTIONS

The addition of the load at the new Cloverleaf delivery point caused potential thermal overloads on the 161 kV systems around Cloverleaf. SPP's solutions consisted of addressing these thermal overloads. The solutions are listed below.

**Solution #1:** Project 1 (Total cost \$1.05M) GRDA cost estimate: \$9.3M

- New W Main to Herron 161 kV line circuit 1

**Solution #2** Project 2 (Total cost \$7.05M) GRDA cost estimate: \$13.8M

- Rebuild W Main to GRDA1 161 kV line circuit 1

SPP chose to move forward with Solution #1. This solution solves all issues identified in Table 3-1 and Table 3-2 in the most cost-effective manner.

**Table 3-4: Recommended Upgrade Solution 1**

| New Upgrade Description*                   | Mileage | MVA (Rate B) | Date Needed** | Host Transmission Owner | Estimated Cost***  |
|--------------------------------------------|---------|--------------|---------------|-------------------------|--------------------|
| New W Main to Herron 161 kV line circuit 1 | 0.5     | 837          | 6/1/2029      | GRDA                    | \$1,050,000        |
| <b>TOTAL NEW UPGRADE COST</b>              |         |              |               |                         | <b>\$1,050,000</b> |

\*All requests with a Network Upgrade(s) identified in the DPNS will be subject to further evaluation in the soonest available Integrated Transmission Planning Assessment that is able to include the load changes, if it is determined that the Network Upgrade(s) will be able to meet the study timeframe requirements pursuant to the standardized project timelines in SPP Business Practices, based on the SPP determined Network Upgrade(s) need date. If it is determined that a Network Upgrade(s) identified from a DPNS is unable to be further evaluated pursuant to the Integrated Transmission Planning Assessment, the DPNS report will be posted on the SPP website once SPP is notified by the Transmission Customer to update the applicable Network Integration Transmission Service Agreement to reflect the changes in delivery points and the Network Upgrade(s).

Pursuant to Attachment AQ of the Tariff, the Transmission provider is responsible for assessing the impacts on the Transmission System caused by modifying an existing delivery point or establishing the new delivery point through the Delivery Point Network Study ("DPNS"). The DPNS may determine the need for a Network Upgrade(s) necessary for the modification of an existing delivery point or the establishment of a new delivery point. A Network Upgrade(s) that the Transmission Customer or Host Transmission Owner desires that exceeds the needed Network Upgrade(s) identified in the DPNS will need to be studied through the Transmission Provider's Sponsored Upgrade study process to evaluate the impacts of the desired changes on the Transmission System.

\*\*If the project need date specified in this study cannot be met, the Transmission Owner will be required to submit mitigations pursuant to the SPP Project Tracking process. All upgrades or mitigations must be in place prior to the dates shown in Table 3-4.

\*\*\*Note that the estimated new upgrade cost provided in this report is an SPP Conceptual Cost Estimate only; this is preliminary, and a more refined Study Cost Estimate will be developed after issuance of this report through a Standardized Cost Estimate Reporting Template (SCERT).

## SECTION 4: CONCLUSION

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The AC analysis revealed potential thermal and voltage violations associated with the Cloverleaf load addition. The study shows that the following upgrades are required to reliably serve the load addition:

- New W Main to Herron 161 kV line circuit 1

The transmission upgrade in Table 3-4 is recommended to mitigate the potential voltage and thermal violations.